# Modified Jaya Optimization Algorithm for Combined Economic Emission Dispatch Solution

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Abstract—The Combined Economic Emission Dispatch (CEED) problem focuses on the short-term determination of optimal generation from a number of power generating units in a way such that both generation costs and emission levels become minimum simultaneously, while satisfying all operational constraints and the load demand. The CEED problem considers the environmental impacts from the gaseous emission of pollutants at fossil-fueled power generating plants. This paper presents the formulation of the CEED problem as a multi-objective problem which in turn has been converted into a single objective function considering price penalty factor. This article proposes a new optimization algorithm, Modified Jaya Optimization Algorithm (MJOA), for CEED problem solution. The existing Jaya Optimization Algorithm (JOA) has been slightly modified to formulate the MJOA for faster convergence and robustness. Later the modified algorithm has been implemented in two test systems to investigate and ensure the effectiveness. The simulation results of the modified algorithm have been compared with other exiting algorithms, present in literature and MJOA has proved to be the best and most powerful amongst them.

*Index Terms*—jaya optimization algorithm, economic load dispatch, constrained minimization, multi objective, valvepoint effect, environmental dispatch

## I. INTRODUCTION

Emission control plays a vital role in energy planning in the field of power system operation and control. Determining optimal generation considering emission and cost constrains simultaneously along with some other system constraints such as valve-point constraint, Prohibited Operating Zone (POZ) etc. is an important practice for Economic Load Dispatch (ELD) problem solution. ELD is an optimization problem in power systems and a process to meet the continuous variation of power demand at minimum operating cost subject to operational constraints. Over the years, various mathematical methods and optimization techniques have been adapted to solve for ELD problems. Lambdaiteration method [1], Gradient method [2], [3], Base-point participation factor method [4] are the conventional optimization methods which have been utilized for ELD problem in the past. These methods have some limitations of high computational time and have several local minima and oscillatory in nature [5]. Recently, some

Stochastic Search Algorithms such as PSO [6]-[11], GA [12]-[14], Direct Search [15] and Differential Evolution [16], [17], Simulated Annealing [18], [19], Gravitational Search [20], [21], Cuckoo Search [22], [23], Binary successive approximation-based evolutionary search [24], [25] have been utilized to solve the ELD problem. However, the above mentioned techniques are associated with its own limitations such as execution speed, executions of many repeated stages, local optimal solution and require common controlling parameters like population size, number of generations etc. Java optimization algorithm [26] is a class of relatively new proposed algorithm. In the present work, Modified Java optimization technique has been applied. It has strong potential to solve the constrained optimization problem. This algorithm requires only the common control parameters and does not require any algorithm specific control parameter.

## II. PROBLEM FORMULATION

The combined environmental economic dispatch problem is to minimize two objective functions, fuel cost and emission, simultaneously while satisfying all equality and inequality constraints. The mathematical formulation of the problem is described as follows.

## A. Economic Dispatch Formulation with Valve Point Effect

The cost function of economic load dispatch problem is defined as follows where  $P_G$  is the total generation:

$$F_{C}(P_{G}) = \sum_{i=1}^{N_{g}} (a_{i} P_{i}^{2} + b_{i} P_{i} + c_{i}) + |d_{i} \sin(e_{i} * (P_{i}^{min} - P_{i}))|$$
(1)

where  $N_g$  is the number of generating units.  $a_i$ ,  $b_i$ ,  $c_i$ ,  $d_i$  and  $e_i$  are the cost coefficients of the  $i^{th}$  generating unit.  $P_i$  is the real power output of the  $i^{th}$  generator.

## B. Emission Dispatch Formulation

The emission function of economic load dispatch problem is defined as follows:

$$E(P_g) = \sum_{i=1}^n 10^{-2} \left( \alpha_i + \beta_i P_{g_i} + \gamma_i P_{g_i}^2 \right) + \xi_i exp(\lambda_i P_{g_i})$$
(2)

where  $\alpha_i$ ,  $\beta_i$ ,  $\gamma_i$ ,  $\xi_i$  and  $\lambda_i$  are coefficients of the *i*<sup>th</sup> generator emission characteristics.

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#### C. Minimization of Fuel Cost and Emission

The multi-objective combined economic and emission problem with its constraints can be mathematically formulated as a nonlinear constrained problem as follows:

$$OF = \omega \sum_{i=1}^{n} F(P_{gi}) + (1 - \omega) \sum_{i=1}^{n} E(P_{gi})$$
(3)

The solution of the problem is achieved by minimizing the objective function (*OF*), the fuel cost rate (\$/h) is shown with F(Pg) and *NOx* emission rate (ton/h) with E(Pgi).

#### D. Power Balance Constraint

Generation should cover the total demand and the active power losses that occur in the transmission system.

$$\sum_{j=1}^{N_g} P_i = P_d + P_{loss} \tag{4}$$

where  $P_d$  is the total demand load and  $P_{loss}$  is the total transmission losses computed using quadratic approximation.

$$P_{loss} = \sum_{i=1}^{Ng} \sum_{j=1}^{Ng} P_i B_{ij} P_j \tag{5}$$

where  $B_{ij}$  is the loss coefficient matrix. This paper assumes *B*-matrix as constant.

Power generation limits. Each unit should generate power within its minimum and maximum limits.

$$P_i^{min} \le P_i \le P_i^{max} \tag{6}$$

## III. JAYA OPTIMIZATION TECHNIQUE

## A. Algorithm and Flowchart

f(x) is assumed as the required objective function which is to be minimized (or maximized). For  $i^{th}$ iteration, the design variables are 'm' numbers (i.e. j =1, 2, ..., m) and 'n' number of candidate solutions which gives the population size, k = 1, 2, ..., n. Amongst entire candidate solutions, the best candidate obtains the best value of f(x) (i.e. say  $f(x)_{best}$ ) and the worst candidateobtains the worst value of f(x) (i.e. say  $f(x)_{worst}$ ). If  $X_{j,k,i}$  is the value of the  $j^{th}$  variable for the  $k^{th}$  member of a set of possible solution during the  $i^{th}$  iteration, then this value is modified as per the following Equation (6):

$$X'_{j,k,i} = X_{j,k,i} + r_{1,j,i} \times (X_{j,best,i} - |X_{j,k,i}|) - r_{2,j,i} \times (X_{j,worst,i} - |X_{j,k,i}|)$$
(7)

where,  $X_{j,best,i}$  is the value of the variable j for the best candidate and  $X_{j,worst,i}$  is the value of the variable j for the worst member of a set of possible solution.  $X'_{j,k,i}$  is the updated value of  $X_{j,k,i}$ . For the  $i^{th}$  iteration in the range of [0, 1],  $r_{1,j,i}$  and  $r_{2,j,i}$  are the two random numbers for the  $j^{th}$  variable. The term " $r_{1,j,i} \times$  $(X_{j,best,i} - |X_{j,k,i}|)$ " shows the affinity of solution to move nearer to the best solution and the term " $r_{2,j,i} \times$  $(X_{j,worst,i} - |X_{j,k,i}|)$ " shows the tendency of the solution to avoid the worst solution.  $X'_{j,k,i}$  is taken into account if it gives better function value. Finally, after iteration, all the accepted function values become the input to the next iteration.

#### B. Flowchart

Fig. 1 shows the flowchart of the Jaya algorithm [26].



Figure 1. Flowchart of the Jaya algorithm

## IV. MODIFICATIONS IN THE ALGORITHM

Current context focusses on one modification in the original Jaya algorithm. The standard Jaya algorithm updates particle's position using the equation (7). This equation uses three terms out of which one term is the current position. In the process of position update, current position is updated to a new position by adding or subtracting a finite value. A minor modification is done in this finite value.

Auxiliary weighted position term: Instead of three terms in equation (7), it uses four terms. The fourth term calculates the fractional value of the mid-position between best and worst positions. This auxiliary weighted term will lead to accelerated convergence which in turn will take less number of iteration count. Less number of iteration count reflects to convergence time without compromising robustness in results. The modified position update equation can be written as-

$$X'_{j,k,i} = X_{j,k,i} + r_{1,j,i} \times (X_{j,best,i} - |X_{j,k,i}|) - r_{2,j,i} \times (X_{j,worst,i} - |X_{j,k,i}|) + r_{3,j,i} \times \{(X_{j,worst,i} + |X_{j,k,i}|)/2\}$$
(8)

where, the fourth term is the Auxiliary weighted position term.

## V. PSEUDO CODE OF JAYA OPTIMIZATION

1. Set i = 1; m = 1; n = 1; j = no. of generators i.e. design variable; k = no. of candidates i.e. population size; P<sup>j</sup><sub>min</sub>= Minimum generation of generators; P<sup>j</sup><sub>max</sub>= Maximum generation of generators;  $P_D$  = Total load demand.

2. Generate initial population i.e. generation of all generators randomly, satisfying all constraints.

**3.** Calculate objective function (cost in \$/hr.)  $C_{T_{ki}}$  (=  $\sum_{i=1}^{J} C_{j,k,i}$ ) for each candidate.

4. WHILE (the termination conditions are not met)

Identify the best solution P<sub>i,best,i</sub> and worst solution P<sub>j,worst,i</sub>

**5.** FOR 
$$m \rightarrow k$$

**FOR**  $n \rightarrow j$ 

Modify solution based on best and worst solutions.

$$\begin{split} P'_{j,k,i} &= P_{j,k,i} + r_{1,j,i} \times (P_{j,best,i} - |P_{j,k,i}|) - r_{2,j,i} \\ &\times (P_{j,worst,i} - |P_{j,k,i}|) + r_{3,j,i} \\ &\times \{(X_{j,worst,i} + |X_{j,k,i}|)/2\} \end{split}$$

## END FOR

**6.** Check whether total generation  $\sum_{j=1}^{j} P'_{j,k,i}$  and demand  $P_D$ are same.

**IF**  $\sum_{i=1}^{j} P'_{j,k,i} \neq P_D$ 

7. Update solutions based on their contribution over total generation.

**FOR**  $n \rightarrow j$ 

$$P''_{j,k,i} = P'_{j,k,i} - \left( \frac{P'_{j,k,i}}{\sum_{j=1}^{j} P'_{j,k,i}} \right) \times \left( \sum_{j=1}^{j} P'_{j,k,i} - P_{D} \right)$$

**8.** Check whether  $P''_{j,k,i}$  is within limits.

 $\textbf{IF} \ P''_{j,k,i} < P^j_{min}$ 

IF P <sub>j,k,i</sub> <  $r_{min}$ P''<sub>j,k,i</sub> =  $P_{min}^{j}$ ELSE IF P''<sub>j,k,i</sub> >  $P_{max}^{j}$ P''<sub>j,k,i</sub> =  $P_{max}^{j}$ 

END **END IF END FOR END IF** 

9. Calculate objective function (cost in hr.)  $C'_{T_{ki}}$  (=  $\sum_{j=1}^{J} C'_{j,k,i}$ ) for each candidate.

10. Check whether  $C'_{T_{k,i}}$  gives better result.

**11. IF**  $C_{T'_{k,i}}$  is better than  $C_{T_{k,i}}$  i.e.  $\sum_{j=1}^{j} C'_{j,k,i} < \sum_{j=1}^{j} C_{j,k,i}$  $C_{T'_{k,i}}^{new} = C_{T'_{k,i}}$ 

 $C_{T_{k_i}}^{new} = C_{T_{k_i}}$ 

**12. ELSE IF**  $C'_{T'_{k,i}}$  is worse than  $C'_{T_{k,i}}$  i.e.  $\sum_{j=1}^{j} C'_{j,k,i} > C'_{T'_{k,i}}$  $\sum_{i=1}^{j}$ 

END **END IF END FOR** 

Set i = i + 1**END WHILE** 

### VI. RESULTS AND DISCUSSIONS

The practical applicability of MJOA has been applied for two case studies (10 and 40 thermal units) where the objective functions were non smooth due to the valvepoint effects.

The MJOA has been applied through coding in MATLAB 7.9.0 (MathWorks, Inc.) and compared with other optimization methods available in literature. All the simulations have been worked out on a 2.2-GHz Intel Pentium processor with 4 GB of RAM.

#### *Case-Study – 1 for 10 Generating Systems* Α.

This case study has been performed for a test system of 10 thermal units considering the effects of valve-point loading. The relevant data for this system has been shown in Table I [27]. In the present study, the load demand is  $P_D = 2000$  MW (considering transmission losses). The results for Case Study-1applying MJOA are shown in Table Π and the program, ELD\_Solution\_Jaya\_Algo\_10\_gen.m, has been written in an m-file. Here the termination criterion has been set as 100 iterations. The m-file has been loaded in the current MATLAB folder. The lower and upper bounds, linear equalities have been set as per the data given in Table I. From successive runs the best results were logged and all the best outputs were written in a tabular form (shown in Table II) for their comparative analysis.

## B. Case-Study – 2 for 40 Generating Systems

A case of 40 thermal units was also carried out to check the effectiveness of the present algorithm. The required data is shown in the Table III [27]. The load demand to be satisfied was  $P_D = 10,500MW$  (without considering transmission losses). To find the optimal generation of power for 40 generating units, the proposed technique has been utilized. The population size, maximum and minimum generation limits and iteration count for the present study has been fixed. The same procedure was followed as in previous case.

The program for MJOA, ELD\_Solution\_Jaya\_Algo\_40\_gen.m, has been written in an MATLAB m-file and kept in the current MATLAB directory. The termination criterion has been set as 2000 iterations. Table IV shows most feasible results for 40 units using different methods. generating The comparative analysis, out of the results in Table IV, puts forth MJOA to be one of the reliable techniques while valve-point effect is considered.

To investigate the effectiveness of this approach, it is seen that in both the two cases the results obtained from MJOA are almost same with the results of other existing methods. From Table II and IV it is seen that MJOA gives viable results in both the cases. For 10 thermal units (Case-study - 1), MJOA decreased the fuel cost as well as total transmission loss. The B-matrix for test system-1 is shown in Box I.

|   | Unit | $P_i^{min}(MW)$ | $P_i^{max}(MW)$ | a <sub>i</sub> (\$/h) | $b_i(\$/MWh)$ | $c_i(\$/(MW)^2h)$ | $d_i(\$/h)$ | e <sub>i</sub> (rad<br>/MW) | $\alpha_i(lb/h)$ | β <sub>i</sub> (lb<br>/MWh) | $\gamma_i(lb/(MW)^2h)$ | $\xi_i(lb/h)$ | $\lambda_{i(1/MW)}$ |
|---|------|-----------------|-----------------|-----------------------|---------------|-------------------|-------------|-----------------------------|------------------|-----------------------------|------------------------|---------------|---------------------|
| ſ | 1    | 10              | 55              | 1000.403              | 40.5407       | 0.12951           | 33          | 0.0174                      | 360.0012         | -3.9864                     | 0.04702                | 0.25475       | 0.01234             |
| ſ | 2    | 20              | 80              | 950.606               | 39.5804       | 0.10908           | 25          | 0.0178                      | 350.0056         | -3.9524                     | 0.04652                | 0.25475       | 0.01234             |
|   | 3    | 47              | 120             | 900.705               | 36.5104       | 0.12511           | 32          | 0.0162                      | 330.0056         | -3.9023                     | 0.04652                | 0.25163       | 0.01215             |
|   | 4    | 20              | 130             | 800.705               | 39.5104       | 0.12111           | 30          | 0.0168                      | 330.0056         | -3.9023                     | 0.04652                | 0.25163       | 0.01215             |
|   | 5    | 50              | 160             | 756.799               | 38.539        | 0.15247           | 30          | 0.0148                      | 13.8593          | 0.3277                      | 0.0042                 | 0.2497        | 0.012               |
|   | 6    | 70              | 240             | 451.325               | 46.1592       | 0.10587           | 20          | 0.0163                      | 13.8593          | 0.3277                      | 0.0042                 | 0.2497        | 0.012               |
| L | 7    | 60              | 300             | 1243.531              | 38.3055       | 0.03546           | 20          | 0.0152                      | 40.2669          | -0.5455                     | 0.0068                 | 0.248         | 0.0129              |
|   | 8    | 70              | 340             | 1049.998              | 40.3965       | 0.02803           | 30          | 0.0128                      | 40.2669          | -0.5455                     | 0.0068                 | 0.2499        | 0.01203             |
|   | 9    | 135             | 470             | 1658.569              | 36.3278       | 0.02111           | 60          | 0.0136                      | 42.8955          | -0.5112                     | 0.0046                 | 0.2547        | 0.01234             |
| L | 10   | 150             | 470             | 1356.659              | 38.2704       | 0.01799           | 40          | 0.0141                      | 42.8955          | -0.5112                     | 0.0046                 | 0.2547        | 0.01234             |
|   |      |                 |                 |                       |               |                   |             |                             |                  |                             |                        |               |                     |
|   |      | L(              | 0.000049        | 0.000014              | 0.000015      | 0.000015 0        | .0000160    | 0.000017                    | 0.000017         | 0.000018                    | 0.000019               | 0.000020      | <sup>C</sup>        |
|   |      | (               | 0.000014        | 0.000045              | 0.000016      | 0.000016 0        | .0000170    | 0.000015                    | 0.000015         | 0.000016                    | 0.000018               | 0.000018      | 3                   |
|   |      | (               | 0.000015        | 0.000016              | 0.000039      | 0.000010 0        | .0000120    | 0.000012                    | 0.000014         | 0.000014                    | 0.000016               | 0.000016      | 5                   |
|   |      | 0               | 0.000015        | 0.000016              | 0.000010      | 0.000040 0        | .0000140    | 0.000010                    | 0.000011         | 0.000012                    | 0.000014               | 0.000015      | 5                   |
|   |      | P = 0           | 0.000016        | 0.000017              | 0.000012      | 0.000014 0        | .0000350    | 0.000011                    | 0.000013         | 0.000013                    | 0.000015               | 0.000016      | 5                   |
|   |      |                 | 0.000017        | 0.000015              | 0.000012      | 0.000010 0        | .0000110    | 0.000036                    | 0.000012         | 0.000012                    | 0.000014               | 0.000015      | 5                   |
|   |      | (               | 0.000017        | 0.000015              | 0.000014      | 0.000011 0        | .0000130    | 0.000012                    | 0.000038         | 0.000016                    | 0.000016               | 0.000018      | 3                   |
|   |      |                 | 0.000018        | 0.000016              | 0.000014      | 0.000012 0        | .0000130    | 0.000012                    | 0.000016         | 0.000040                    | 0.000015               | 0.000016      | 5                   |

TABLE I.DATA FOR THE 10 THERMAL UNITS [27]

BOX I. TRANSMISSION LOSS MATRIX FOR TEST SYSTEM

0.000016 0.000014 0.0000150.000014 0.000016 0.000015

0.000016 0.000015 0.0000160.000015 0.000018 0.000016

0.000042

0.000019

0.000019

0.000044

TABLE II. COMPARISON OF BEST RESULTS OF DIFFERENT OPTIMIZATION TECHNIQUES FOR CASE STUDY-1, PD = 2000 MW

| Comparison of the results for test system-1 ( $P_D = 2000 \text{ MW}$ ) |              |          |                 |              |           |           |           |           |  |  |
|---|--------------|----------|-----------------|--------------|-----------|-----------|-----------|-----------|--|--|
| Unit  | MODE<br>[27] | PDE [27] | NSGA-II<br>[27] | SPEA<br>[27] | GSA [28]  | TLBO      | JOA       | MJOA      |  |  |
| P1(MW)  | 54.9487      | 54.9853  | 51.9515         | 52.9761      | 54.9992   | 54.4285   | 55.0000   | 54.9441   |  |  |
| P2(MW)  | 74.5821      | 79.3803  | 67.2584         | 72.8130      | 79.9586   | 78.9558   | 78.4112   | 79.7300   |  |  |
| P3(MW)  | 79.4294      | 83.9842  | 73.6879         | 78.1128      | 79.4341   | 79.5993   | 80.3464   | 80.1338   |  |  |
| P4(MW)  | 80.6875      | 86.5942  | 91.3554         | 83.6088      | 85.0000   | 85.4390   | 84.6690   | 86.2269   |  |  |
| P5(MW)  | 136.8551     | 144.4386 | 134.0522        | 137.2432     | 142.1063  | 143.7134  | 143.8600  | 143.5906  |  |  |
| P6(MW)  | 172.6393     | 165.7756 | 174.9504        | 172.9188     | 166.5670  | 166.9796  | 167.4608  | 165.9426  |  |  |
| P7(MW)  | 283.8233     | 283.2122 | 289.4350        | 287.2023     | 292.8749  | 293.3021  | 292.4104  | 292.7701  |  |  |
| P8(MW)  | 316.3407     | 312.7709 | 314.0556        | 326.4023     | 313.2387  | 312.9163  | 313.2630  | 312.4573  |  |  |
| P9(MW)  | 448.5923     | 440.1135 | 455.6978        | 448.8814     | 441.1775  | 440.4352  | 440.4677  | 440.3041  |  |  |
| P10(MW)   | 436.4287     | 432.6783 | 431.8054        | 423.9025     | 428.6306  | 428.1624  | 428.0384  | 427.8155  |  |  |
| Cost ( x 10^5 \$)   | 1.1348       | 1.1351   | 1.1354          | 1.1352       | 1.1349    | 1.1333    | 1.1333    | 1.1330    |  |  |
| Emission (lb)   | 4124.9       | 4111.4   | 4130.2          | 4109.1       | 4111.4000 | 4108.1000 | 4105.3000 | 4108.8000 |  |  |
| Loss (MW)   | 84.3271      | 83.9331  | 84.2496         | 84.0612      | 83.9869   | 83.9317   | 83.9270   | 83.9150   |  |  |

 TABLE III.
 Data for the 40 Thermal Units [27]

| Unit | $P_i^{min}(MW)$ | $P_i^{max}(MW)$ | $a_i(\$/h)$ | $b_i  (\$/MWh)$ | $c_i(\$/(MW)^2h)$ | $d_i(\$/h)$ | e <sub>i</sub> (rad/MW) | $\alpha_i(ton/h)$ | β <sub>i</sub> (ton<br>/MWh) | $\gamma_i(ton / (MW)^2 h)$ | $\xi_i(ton/h)$ | $\lambda_i (1/MW)$ |
|------|-----------------|-----------------|-------------|-----------------|-------------------|-------------|-------------------------|-------------------|------------------------------|----------------------------|----------------|--------------------|
| 1    | 36              | 114             | 94.705      | 6.73            | 0.0069            | 100         | 0.084                   | 60                | -2.22                        | 0.048                      | 1.31           | 0.0569             |
| 2    | 36              | 114             | 94.705      | 6.73            | 0.0069            | 100         | 0.084                   | 60                | -2.22                        | 0.048                      | 1.31           | 0.0569             |
| 3    | 60              | 120             | 309.54      | 7.07            | 0.02028           | 100         | 0.084                   | 100               | -2.36                        | 0.0762                     | 1.31           | 0.0569             |
| 4    | 80              | 190             | 369.03      | 8.18            | 0.00942           | 150         | 0.063                   | 120               | -3.14                        | 0.054                      | 0.9142         | 0.0454             |
| 5    | 47              | 97              | 148.89      | 5.35            | 0.0114            | 120         | 0.077                   | 50                | -1.89                        | 0.085                      | 0.9936         | 0.0406             |
| 6    | 68              | 140             | 222.33      | 8.05            | 0.01142           | 100         | 0.084                   | 80                | -3.08                        | 0.0854                     | 1.31           | 0.0569             |
| 7    | 110             | 300             | 287.71      | 8.03            | 0.00357           | 200         | 0.042                   | 100               | -3.06                        | 0.0242                     | 0.655          | 0.02846            |
| 8    | 135             | 300             | 391.98      | 6.99            | 0.00492           | 200         | 0.042                   | 130               | -2.32                        | 0.031                      | 0.655          | 0.02846            |
| 9    | 135             | 300             | 455.76      | 6.6             | 0.00573           | 200         | 0.042                   | 150               | -2.11                        | 0.0335                     | 0.655          | 0.02846            |
| 10   | 130             | 300             | 722.82      | 12.9            | 0.00605           | 200         | 0.042                   | 280               | -4.34                        | 0.425                      | 0.655          | 0.02846            |
| 11   | 94              | 375             | 635.2       | 12.9            | 0.00515           | 200         | 0.042                   | 220               | -4.34                        | 0.0322                     | 0.655          | 0.02846            |
| 12   | 94              | 375             | 654.69      | 12.8            | 0.00569           | 200         | 0.042                   | 225               | -4.28                        | 0.0338                     | 0.655          | 0.02846            |
| 13   | 125             | 500             | 913.4       | 12.5            | 0.00421           | 300         | 0.035                   | 300               | -4.18                        | 0.0296                     | 0.5035         | 0.02075            |
| 14   | 125             | 500             | 1760.4      | 8.84            | 0.00752           | 300         | 0.035                   | 520               | -3.34                        | 0.0512                     | 0.5035         | 0.02075            |
| 15   | 125             | 500             | 1760.4      | 8.84            | 0.00752           | 300         | 0.035                   | 510               | -3.55                        | 0.0496                     | 0.5035         | 0.02075            |
| 16   | 125             | 500             | 1760.4      | 8.84            | 0.00752           | 300         | 0.035                   | 510               | -3.55                        | 0.0496                     | 0.5035         | 0.02075            |
| 17   | 220             | 500             | 647.85      | 7.97            | 0.00313           | 300         | 0.035                   | 220               | -2.68                        | 0.0151                     | 0.5035         | 0.02075            |
| 18   | 220             | 500             | 649.69      | 7.95            | 0.00313           | 300         | 0.035                   | 222               | -2.66                        | 0.0151                     | 0.5035         | 0.02075            |
| 19   | 242             | 550             | 647.83      | 7.97            | 0.00313           | 300         | 0.035                   | 220               | -2.68                        | 0.0151                     | 0.5035         | 0.02075            |
| 20   | 242             | 550             | 647.81      | 7.97            | 0.00313           | 300         | 0.035                   | 220               | -2.68                        | 0.0151                     | 0.5035         | 0.02075            |

0.000019 0.000018

L<sub>0.000020</sub> 0.000018

| 21 | 254 | 550 | 785.96 | 6.63 | 0.00298 | 300 | 0.035 | 290 | -2.22 | 0.0145 | 0.5035 | 0.02075 |
|----|-----|-----|--------|------|---------|-----|-------|-----|-------|--------|--------|---------|
| 22 | 254 | 550 | 785.96 | 6.63 | 0.00298 | 300 | 0.035 | 285 | -2.22 | 0.0145 | 0.5035 | 0.02075 |
| 23 | 254 | 550 | 794.53 | 6.66 | 0.00284 | 300 | 0.035 | 295 | -2.26 | 0.0138 | 0.5035 | 0.02075 |
| 24 | 254 | 550 | 794.53 | 6.66 | 0.00284 | 300 | 0.035 | 295 | -2.26 | 0.0138 | 0.5035 | 0.02075 |
| 25 | 254 | 550 | 801.32 | 7.1  | 0.00277 | 300 | 0.035 | 310 | -2.42 | 0.0132 | 0.5035 | 0.02075 |
| 26 | 254 | 550 | 801.32 | 7.1  | 0.00277 | 300 | 0.035 | 310 | -2.42 | 0.0132 | 0.5035 | 0.02075 |
| 27 | 10  | 150 | 1055.1 | 3.33 | 0.52124 | 120 | 0.077 | 360 | -1.11 | 1.842  | 0.9936 | 0.0406  |
| 28 | 10  | 150 | 1055.1 | 3.33 | 0.52124 | 120 | 0.077 | 360 | -1.11 | 1.842  | 0.9936 | 0.0406  |
| 29 | 10  | 150 | 1055.1 | 3.33 | 0.52124 | 120 | 0.077 | 360 | -1.11 | 1.842  | 0.9936 | 0.0406  |
| 30 | 47  | 97  | 148.89 | 5.35 | 0.0114  | 120 | 0.077 | 50  | -1.89 | 0.085  | 0.9936 | 0.0406  |
| 31 | 60  | 190 | 222.92 | 6.43 | 0.0016  | 150 | 0.063 | 80  | -2.08 | 0.0121 | 0.9142 | 0.0454  |
| 32 | 60  | 190 | 222.92 | 6.43 | 0.0016  | 150 | 0.063 | 80  | -2.08 | 0.0121 | 0.9142 | 0.0454  |
| 33 | 60  | 190 | 222.92 | 6.43 | 0.0016  | 150 | 0.063 | 80  | -2.08 | 0.0121 | 0.9142 | 0.0454  |
| 34 | 90  | 200 | 107.87 | 8.95 | 0.0001  | 200 | 0.042 | 65  | -3.48 | 0.0012 | 0.655  | 0.02846 |
| 35 | 90  | 200 | 116.58 | 8.62 | 0.0001  | 200 | 0.042 | 70  | -3.24 | 0.0012 | 0.655  | 0.02846 |
| 36 | 90  | 200 | 116.58 | 8.62 | 0.0001  | 200 | 0.042 | 70  | -3.24 | 0.0012 | 0.655  | 0.02846 |
| 37 | 25  | 110 | 307.45 | 5.88 | 0.0161  | 80  | 0.098 | 100 | -1.98 | 0.095  | 1.42   | 0.0677  |
| 38 | 25  | 110 | 307.45 | 5.88 | 0.0161  | 80  | 0.098 | 100 | -1.98 | 0.095  | 1.42   | 0.0677  |
| 39 | 25  | 110 | 307.45 | 5.88 | 0.0161  | 80  | 0.098 | 100 | -1.98 | 0.095  | 1.42   | 0.0677  |
| 40 | 242 | 550 | 647.83 | 7.97 | 0.00313 | 300 | 0.035 | 220 | -2.68 | 0.0151 | 0.5035 | 0.02075 |

TABLE IV. COMPARISON OF BEST RESULTS OF DIFFERENT OPTIMIZATION TECHNIQUES FOR CASE STUDY-2, PD=10,500 MW

| Comparison of the results for test system 2 ( $PD = 10,500 \text{ MW}$ ) |           |          |                 |           |          |          |          |  |  |  |  |
|--|-----------|----------|-----------------|-----------|----------|----------|----------|--|--|--|--|
| Unit   | MODE [27] | PDE [27] | NSGA-II<br>[27] | SPEA [27] | GSA [28] | TLBO     | MJOT     |  |  |  |  |
| P1(MW)   | 113.5295  | 112.1549 | 113.8685        | 113.9694  | 113.9989 | 113.9637 | 113.7032 |  |  |  |  |
| P2(MW)   | 114       | 113.9431 | 113.6381        | 114       | 113.9896 | 114.0000 | 114.0000 |  |  |  |  |
| P3(MW)   | 120       | 120      | 120             | 119.8719  | 119.9995 | 119.2759 | 119.9368 |  |  |  |  |
| P4(MW)   | 179.8015  | 180.2647 | 180.7887        | 179.9284  | 179.7857 | 181.0562 | 180.5315 |  |  |  |  |
| P5(MW)   | 96.7716   | 97       | 97              | 97        | 97       | 96.4756  | 97.0000  |  |  |  |  |
| P6(MW)   | 139.276   | 140      | 140             | 139.2721  | 139.0128 | 137.7332 | 138.3124 |  |  |  |  |
| P7(MW)   | 300       | 299.8829 | 300             | 300       | 299.9885 | 299.4274 | 300.0000 |  |  |  |  |
| P8(MW)   | 298.9193  | 300      | 299.0084        | 298.2706  | 300      | 299.6958 | 300.0000 |  |  |  |  |
| P9(MW)   | 290.7737  | 289.8915 | 288.889         | 290.5228  | 296.2025 | 298.0269 | 297.1393 |  |  |  |  |
| P10(MW)  | 130.9025  | 130.5725 | 131.6132        | 131.4832  | 130.385  | 131.0000 | 130.9194 |  |  |  |  |
| P11(MW)  | 244.7349  | 244.1003 | 246.5128        | 244.6704  | 245.4775 | 245.1809 | 245.2199 |  |  |  |  |
| P12(MW)  | 317.8218  | 318.284  | 318.8748        | 317.2003  | 318.2101 | 319.6045 | 318.0639 |  |  |  |  |
| P13(MW)  | 395.3846  | 394.7833 | 395.7224        | 394.7357  | 394.6257 | 394.8243 | 394.2374 |  |  |  |  |
| P14(MW)  | 394.4692  | 394.2187 | 394.1369        | 394.6223  | 395.2016 | 395.6854 | 396.4756 |  |  |  |  |
| P15(MW)  | 305.8104  | 305.9616 | 305.5781        | 304.7271  | 306.0014 | 306.6104 | 306.8609 |  |  |  |  |
| P16(MW)  | 394.8229  | 394.1321 | 394.6968        | 394.7289  | 395.1005 | 393.7669 | 393.9455 |  |  |  |  |
| P17(MW)  | 487.9872  | 489.304  | 489.4234        | 487.9857  | 489.2569 | 489.3632 | 489.8599 |  |  |  |  |
| P18(MW)  | 489.1751  | 489.6419 | 488.2701        | 488.5321  | 488.7598 | 489.2599 | 488.5698 |  |  |  |  |
| P19(MW)  | 500.5265  | 499.9835 | 500.8           | 501.1683  | 499.232  | 499.3462 | 497.9881 |  |  |  |  |
| P20(MW)  | 457.0072  | 455.416  | 455.2006        | 456.4324  | 455.2821 | 455.8277 | 454.8535 |  |  |  |  |
| P21(MW)  | 434.6068  | 435.2845 | 434.6639        | 434.7887  | 433.452  | 433.3401 | 432.5556 |  |  |  |  |
| P22(MW)  | 434.531   | 433.7311 | 434.15          | 434.3937  | 433.8125 | 432.5457 | 434.2654 |  |  |  |  |
| P23(MW)  | 444.6732  | 446.2496 | 445.8385        | 445.0772  | 445.5136 | 445.5808 | 444.7076 |  |  |  |  |
| P24(MW)  | 452.0332  | 451.8828 | 450.7509        | 451.897   | 452.0547 | 453.4598 | 452.8684 |  |  |  |  |
| P25(MW)  | 492.7831  | 493.2259 | 491.2745        | 492.3946  | 492.8864 | 493.0912 | 492.2676 |  |  |  |  |
| P26(MW)  | 436.3347  | 434.7492 | 436.3418        | 436.9926  | 433.3695 | 434.2457 | 434.1368 |  |  |  |  |
| P27(MW)  | 10        | 11.8064  | 11.2457         | 10.7784   | 10.0026  | 11.2841  | 10.7532  |  |  |  |  |
| P28(MW)  | 10.3901   | 10.7536  | 10              | 10.2955   | 10.0246  | 10.6029  | 11.1086  |  |  |  |  |
| P29(MW)  | 12.3149   | 10.3053  | 12.0714         | 13.7018   | 10.0125  | 10.9478  | 11.1915  |  |  |  |  |
| P30(MW)  | 96.905    | 97       | 97              | 96.2431   | 96.9125  | 96.2683  | 97.0000  |  |  |  |  |
| P31(MW)  | 189.7727  | 190      | 189.4826        | 190       | 189.9689 | 189.5610 | 189.2526 |  |  |  |  |
| P32(MW)  | 174.2324  | 175.3065 | 174.7971        | 174.2163  | 175      | 174.3280 | 174.6346 |  |  |  |  |
| P33(MW)  | 190       | 190      | 189.2845        | 190       | 189.0181 | 188.7028 | 188.8095 |  |  |  |  |
| P34(MW)  | 199.6506  | 200      | 200             | 200       | 200      | 198.2413 | 200.0000 |  |  |  |  |
| P35(MW)  | 199.8662  | 200      | 199.9138        | 200       | 200      | 198.3432 | 198.6563 |  |  |  |  |
| P36(MW)  | 200       | 200      | 199.5066        | 200       | 199.9978 | 200.2483 | 200.4569 |  |  |  |  |
| P37(MW)  | 110       | 109.9412 | 108.3061        | 110       | 109.9969 | 109.5386 | 109.4282 |  |  |  |  |
| P38(MW)  | 109.9454  | 109.8823 | 110             | 109.6912  | 109.0126 | 108.7831 | 110.0000 |  |  |  |  |
| P39(MW)  | 108.1786  | 108.9686 | 109.7899        | 108.556   | 109.456  | 110.0000 | 108.5079 |  |  |  |  |
| P40(MW)  | 422.0682  | 421.3778 | 421.5609        | 421.8521  | 421.9987 | 420.7631 | 421.7822 |  |  |  |  |
| Cost (X 10^5 \$)   | 1.2579    | 1.2573   | 1.2583          | 1.2581    | 1.2578   | 1.2323   | 1.2322   |  |  |  |  |
| Emission (lb)  |           |          |                 |           |          |          |          |  |  |  |  |
| (X 10^5 ton)   | 2.1119    | 2.1177   | 2.1095          | 2.111     | 2.1093   | 2.114    | 2.103    |  |  |  |  |

In case study-2 (Test system-2) MJOA has worked effectively decreasing both generation cost and emission.

## VII. CONCLUSION

Jaya Optimization Algorithm (JOA) is one of the recent powerful methods for solving constrained optimization problems. The present work proposed a new approach for minimizing the generating cost in electric power industry. The successful implementation of MJOA brings forth robust solutions for multi-objective problem solution. CEED problem consists of non-smooth cost function which has been successfully solved by MJOA considering two test systems. The results, associated with two different systems (10 thermal units and 40 thermal units), achieved with the application of MJOA have been compared and analyzed with other existing methods available in literature. The performance of MJOA proved to be effective while satisfying the constraints with highly probable solutions in an acceptable computing time. MJOA has therefore proved to be capable of providing better results when compared with other stochastic search algorithms and hence stands to be a very effective technique to solve ELD problems.

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